





# Common Natural Gas Engineering Problems – And Solutions

Ohio Gas Association  
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## DISCLAIMER

Some portions of 49 CFR Part 192 are open to interpretation and federal or state regulators may not agree with the opinions expressed in this seminar. Attendees are urged to research the facts and arrive at their own conclusions.

## Steel Pipe Design:

- Design formula for steel pipe
- Other design considerations
- Additional design requirements for using an alternate MAOP
- Specifications when ordering steel pipe
- Record keeping for steel pipe
- Double stamped pipe

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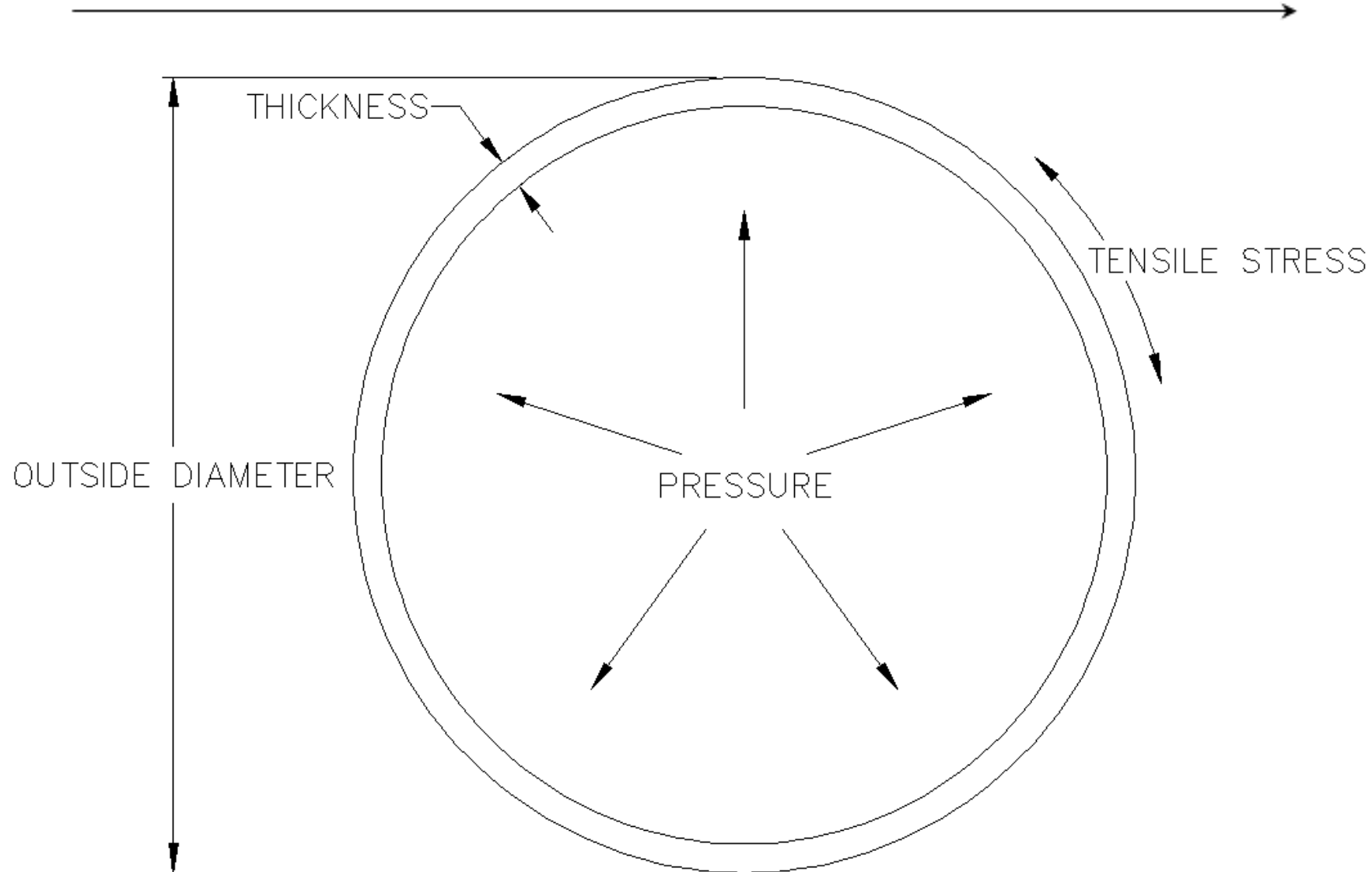
## Tensile Stress:

- A force that attempts to pull apart or stretch a material



## Tensile Strength:

- A materials ability to resist tensile stress



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## Barlow's formula: $P = 2St/D$

Tells us that the Tensile Stress (which is also called the Hoop Stress) on the pipe = Pressure x Outside Diameter / 2 x Thickness, i.e.  $S = PD/(2t)$

SO,

$1000 \text{ psig} \times 10.75 \text{ in} / (2 \times 0.250 \text{ in}) = 21,500 \text{ psig}$  tensile stress

$2000 \text{ psig} \times 10.75 \text{ in} / (2 \times 0.250 \text{ in}) = 43,000 \text{ psig}$  tensile stress

And yes, size does matter!!

$2000 \text{ psig} \times 20.00 \text{ in} / (2 \times 0.250 \text{ in}) = 80,000 \text{ psig}$  tensile stress

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## How much tensile stress can we put on pipe?

For our purposes:

- Maximum tensile/hoop stress allowed in pipe  $\approx$  Yield Strength “S”, or Specified Minimum Yield Strength, “SMYS”
  - Grade A = 25,000 psi
  - Grade B = 35,000 psi
  - API 5L X-42 = 42,000 psi
  - API 5L X-52 = 52,000 psi
  - API 5L X-60 = 60,000 psi
  - API 5L X-65 = 65,000 psi
- Pipe used for projects regulated under Part 192 must be a listed specification in 192.7



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## 192.105 Design Formula for Steel Pipe

$$P = (2St/D) \times F \times E \times T$$

- Design Pressure “P”
- Yield Strength (or SMYS) “S”
- Nominal Wall Thickness “t”
- Nominal Outside Diameter “D”
- Design Factor “F”
- Longitudinal Joint Factor “E”
- Temperature De-rating Factor “T”

Design Factor “F” is our safety factor

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## 192.105 Design Formula for Steel Pipe

$$P = (2St/D) \times F \times E \times T$$

- Step 1: Choose a pipe and enter “S” (Yield Strength), “t” (Wall Thickness), and “D” (Outside Diameter)
  - For new pipe this should be straight forward
  - For existing pipe, you need to rely on existing records. If “S” is unknown, use 24,000 psi or determine “S” in accordance with Section II-D of Appendix B
  - If “t” is unknown, it must be determined in accordance with 192.109

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$$P = (2St/D) \times F \times E \times T$$

- Step 2: Determine the Design Factor “F”
  - Class 1 Locations,  $F = 0.72$
  - Class 2 Locations,  $F = 0.60$
  - Class 3 Locations,  $F = 0.50$
  - Class 4 Locations,  $F = 0.40$
  - Exceptions: 0.60 for pipe in Class 1 Locations that (1) Cross the right-of-way of an unimproved public road without casing; (2) Crosses without a casing, or makes a parallel encroachment on, the right-of-way of either a hard surfaced road, a highway, a public street, or a railroad; (3) Is supported by a vehicular, pedestrian, railroad, or pipeline bridge.

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$$P = (2St/D) \times F \times E \times T$$

- Step 2: Determine the Design Factor “F”
  - Class 1 Locations,  $F = 0.72$
  - Exception: 0.60 for pipe in Class 1 Locations that (4) Is used in a fabricated assembly, (including separators, mainline valve assemblies, cross-connections, and river crossing headers) or is used within five pipe diameters in any direction from the last fitting of a fabricated assembly, other than a transition piece or an elbow used in place of a pipe bend which is not associated with a fabricated assembly.

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$$P = (2St/D) \times F \times E \times T$$

- Step 2: Determine the Design Factor “F”
  - Class 1 Locations,  $F = 0.72$
  - Class 2 Locations,  $F = 0.60$
  - Exception: For Class 2 locations, a design factor of 0.50, or less, must be used ... for uncased steel pipe that crosses the right-of-way of a hard surfaced road, a highway, a public street, or a railroad.
  - Exception: For Class 1 and Class 2 locations, a design factor of 0.50, or less, must be used ... in a compressor station, regulating station, or measuring station

$$P = (2St/D) \times F \times E \times T$$

- Step 3: Longitudinal Joint Factor “E”

Specification	Pipe Class	Longitudinal Joint Factor (E)
ASTM A53/A53M	Seamless	1.00
	Electric Resistance Welded	1.00
	Furnace Butt Welded	0.60
ASTM A106	Seamless	1.00
~	~	~
API 5L	Seamless	1.00
	Electric Resistance Welded	1.00
	Electric Flash Welded	1.00
	Submerged Arc Welded	1.00
	Furnace Butt Welded	0.60
Other	Pipe over 4 inches	0.80
Other	Pipe 4 inches and less	0.60

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$$P = (2St/D) \times F \times E \times T$$

- Step 4: Temperature De-rating Factor “T”
  - For gas temperature below 250° F = 1.000
  - For gas temperature above 250° F, see 192.115

# Examples

What's the design pressure for 12", API 5L X-42, 0.250w, ERW, in a Class 3 location?

$$P = (2St/D) \times F \times E \times T$$

$$P = 2 \times 42,000 \times 0.250 / 12.75 \times 0.50 \times 1.00 \times 1.00$$

$$P = 823.53 \text{ psig} \leftarrow$$

What wall thickness do I need for a 20", API 5L X-52, ERW, Class 1 road crossing if I want a 1000 psig MAOP?

$$P = 2 \times 52,000 \times 0.250 / 20.00 \times 0.60 \times 1.00 \times 1.00 = 780 \text{ psig}$$

$$P = 2 \times 52,000 \times 0.320512821 / 20.00 \times 0.60 \times 1.00 \times 1.00 = 1000 \text{ psig}$$

$$P = 2 \times 52,000 \times 0.375 / 20.00 \times 0.60 \times 1.00 \times 1.00 = 1170 \text{ psig} \leftarrow$$

For other pipe besides road crossings and valve settings:

$$P = 2 \times 60,000 \times 0.250 / 20.00 \times 0.72 \times 1.00 \times 1.00 = 1080 \text{ psig} \leftarrow$$



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- Other Considerations

- Distribution vs. Transmission (need to keep below 20% SMYS)

How do I calculate 20% SMYS?

12", API 5L X-42, 0.250w, ERW. SMYS = 42,000

20% of 42,000 =  $0.2 \times 42,000 = 8400$  psi

Use Barlow's formula:  $P = 2St/D$  (do NOT use E, F, or T)

$P = 2 \times 8400 \times 0.250 / 12.75 = 329.41$  psig←

Class 3 design =  $2 \times 42,000 \times 0.250 / 12.75 \times 0.50 \times 1 \times 1 = 823$  psig

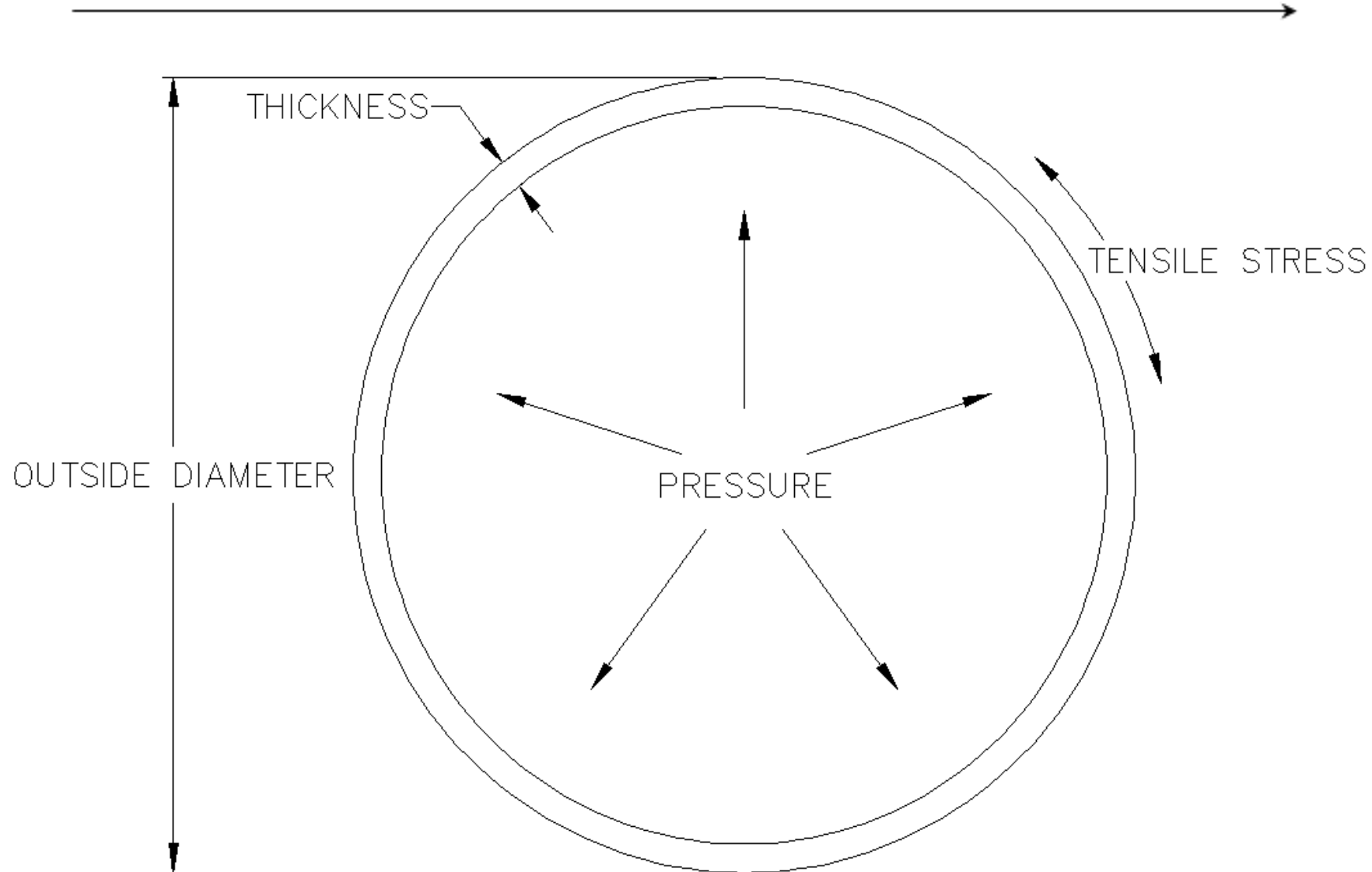
But anything over 329 MAOP will cause it to be a transmission line

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- Other Considerations

- Availability of fittings
- Future Class location changes
- Road, railroad crossings
- Bridges
- Compressor, regulator/meter stations, valve settings, other above ground facilities
- Damage prevention
- Corrosion allowance
- Ohio Power Siting Requirements
- External loading

External loading on the pipe is additive and must be considered separately using API 1102 or other external loading calculations



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## Additional requirements for alternative MAOP

- Allows for Design Factor “F” up to 0.80 in Class 1, 0.67 in Class 2, and 0.56 in Class 3
- Significant additional requirements for almost every aspect, including pipe manufacturing, design, construction, testing, and operations and maintenance
- See 192.112 for further details

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## Specifications for ordering steel pipe

- Diameter
- Pipe manufacturing specifications
- Grade
- Wall thickness
- Product Specification Level (PSL) for API 5L pipe

Current reference standard in Part 192.7 is ANSI/API Specification 5L/ISO 3183 “Specification for Line Pipe”, 44<sup>th</sup> edition, 2007, including January 2009 errata and February 2009 Addendum 1



### Summary of Differences Between PSL 1 and PSL 2

Parameter	PSL1	PSL2
Grade range	A25 through X70	B through X80
Size range	0.405 through 80	4.5 through 80
Type of pipe ends	Plain-end, threaded end	Plain-end
Seam welding	All methods: continuous welding limited to Grade A25	All methods except continuous and laser welding
Electric welds: welder frequency	No minimum	100kHz minimum
Heat treatment of electric welds	Required for grades > X42	Required for all grades (B through X80)
Chemistry: max C for seamless pipe	0.28% for grades $\geq$ B	0.24%
Chemistry: max C for welded pipe	0.26% for grades $\geq$ B	0.22%
Chemistry: max P	0.030% for grades $\geq$ A	0.025%
Chemistry: max S	0.030%	0.015%
Carbon equivalent	Only when purchaser specifies SR18	Maximum required for each grade
Yield Strength, maximum	None	Maximum required for each grade
UTS, maximum	None	Maximum required for each grade
Fracture toughness	None required	Required for all grades
Nondestructive inspection of seamless	Only when purchaser specifies SR4	SR4 mandatory
Repair by welding of pipe body, plate by skelp	Permitted	Prohibited
Repair by welding of weld seams without filler metal	Permitted by agreement	Prohibited
Certification	Certificates when specified per SR15	Certificates (SR 15.1) mandatory
Traceability	Traceable only until all tests are passed, unless SR15 is specified	Traceable after completion of tests (SR 15.2) mandatory

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## Record Keeping for Steel Pipe

- Purchase orders (vs. phone call)
- Invoice
- Shipping receipt/bill of lading
- Mill test report (MTR's)
- Documentation on where pipe was actually installed

MTR's should be requested and retained whenever possible



## CERTIFICATE OF TESTING IPSCO TUBULARS (KY) INC

Page 2

Certificate Number:	184425-4
Friday, February 18, 2011, 10:34:38 AM	

Diameter: 16.00 in	Gage: 0.375 in	Grade: X42/52-2M	MIR Order No:	Customer POC														
Specification: API 5L FORTY-FOURTH EDITION GRADES X42X52 PSL2		Customer: QAC STOCK																
Heat	Product ID	Test Type		Orientation				Width (in)		YS (psi)		UTS (psi)		Elong%(2 in)		Y/T		
		Wgt (%)	C	Min	P	S	SI	Cu	NI	Cr	Mo	Sn	Al	V	Co	Ti	B	PCM
B115441	WL-H72 970	Product:	0.08	1.12	0.011	0.004	0.22	0.07	0.03	0.03	0.008	0.005	0.026	0.002	0.041	0.01	0.0002	0.13
	WL-H72 970B	Product:	0.08	1.12	0.011	0.004	0.22	0.07	0.03	0.03	0.008	0.005	0.026	0.002	0.041	0.01	0.0001	0.13
B115442	WL-H72 964	MILL CONTROL	PIPE TPA				1.509		64000		75900		38.0		0.84			
	WL-H72 964B	MILL CONTROL	PIPE TPA				1.518		64100		75700		38.0		0.85			
	WL-H72 964W	MILL CONTROL	PIPE TWA				1.514				80300		0.0		0.08			
	WL-H72 964WB	MILL CONTROL	PIPE TWA				1.517				81500		0.0		0.00			
		Heats:	0.03	1.09	0.010	0.001	0.22	0.07	0.02	0.03	0.011	0.001	0.030	0.001	0.045	0.01	0.0005	0.10
WL-H72 984	Product:	0.08	1.09	0.011	0.004	0.22	0.08	0.03	0.03	0.009	0.006	0.025	0.002	0.039	0.01	0.0001	0.12	
	WL-H72 984B	Product:	0.08	1.10	0.011	0.003	0.22	0.08	0.03	0.03	0.009	0.005	0.026	0.002	0.039	0.01	0.0001	0.12
B115443	WL-H72 988	MILL CONTROL	PIPE TPA				1.508		66600		77100		40.0		0.88			
	WL-H72 988B	MILL CONTROL	PIPE TPA				1.503		65200		76500		39.0		0.88			
	WL-H72 988W	MILL CONTROL	PIPE TWA				1.507				78300		0.0		0.00			
	WL-H72 988WB	MILL CONTROL	PIPE TWA				1.514				77800		0.0		0.06			
		Heats:	0.04	1.12	0.011	0.001	0.25	0.08	0.02	0.03	0.011	0.002	0.034	0.001	0.046	0.01	0.0005	0.11
WL-H72 988	Product:	0.08	1.12	0.012	0.003	0.24	0.09	0.03	0.04	0.009	0.008	0.029	0.002	0.040	0.01	0.0001	0.12	
	WL-H72 988B	Product:	0.08	1.13	0.011	0.002	0.24	0.09	0.03	0.04	0.009	0.008	0.030	0.002	0.040	0.01	0.0001	0.13
B115448	WL-H72 973	MILL CONTROL	PIPE TPA				1.512		87000		77500		40.0		0.86			
	WL-H72 973B	MILL CONTROL	PIPE TPA				1.510		68700		79000		40.0		0.87			
	WL-H72 973W	MILL CONTROL	PIPE TWA				1.518				81800		0.0		0.09			
	WL-H72 973WB	MILL CONTROL	PIPE TWA				1.513				81500		0.0		0.08			
		Heats:	0.04	1.09	0.009	0.001	0.22	0.08	0.03	0.03	0.013	0.002	0.033	0.001	0.046	0.01	0.0005	0.11
WL-H72 973	Product:	0.08	1.10	0.011	0.003	0.22	0.09	0.04	0.04	0.012	0.008	0.031	0.003	0.040	0.01	0.0002	0.13	
	WL-H72 973B	Product:	0.08	1.10	0.011	0.003	0.22	0.09	0.04	0.04	0.012	0.008	0.030	0.002	0.040	0.01	0.0001	0.13
B115446	WL-H72 988	MILL CONTROL	PIPE TPA				1.510		66800		77300		40.0		0.86			
	WL-H72 868B	MILL CONTROL	PIPE TPA				1.511		64700		76400		40.0		0.85			

LA - Transverse Pipe Axis  
 LPA - Longitudinal Pipe Axis  
 TWA - Transverse Weld Axis  
 FST - Full Section Testing  
 PBT - Flat Body Nondestructive  
 Q&T - Quenched and Tempered  
 SH - Stress Relieved  
 Item: CRTX0001

Flattening Test Acceptable  
 Ultrasonic Weld Line Inspection Acceptable  
 Electric Resistance Welded (Type II)  
 UT Cal. to 1/8" Orificed Hole and/or NID (RVD) Notches  
 Milled and Manufactured in the USA  
 Hydrostatic Test Pressure: 1720 PSI for 5secs  
 Minimum Weld Seam Heat Treatment Temperature: 1800 (F)

We certify that the product described above has been manufactured, sampled, inspected, and tested in accordance to the referenced specification. The product has been found to be in compliance with all requirements.

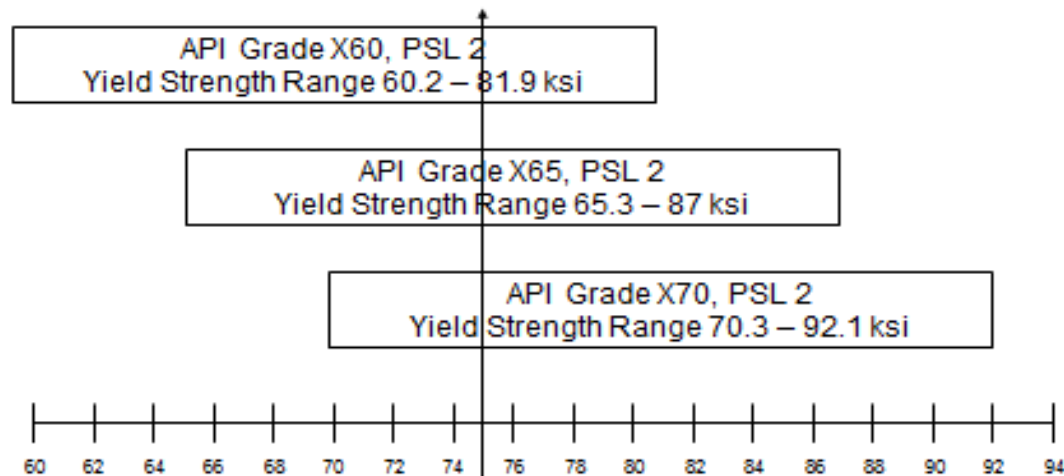
Thursday, June 16, 2011, 7:00:16 AM

MILL ADDRESS - 100 STEEL PLANT RD | WILDER, KY 41071



# Double Stamped Pipe

- Why double stamped pipe?



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The most common dual grade product has been Grade B/X42, but other common dual-grades are:

X-42/X-46

Grade B/X-42/X-46

X-42/X-52

X-60/X-65

X-60/X-65/X-70

UTi's policy is to design to any single chosen grade but to weld to the highest stamped grade.

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## Steel Pipe Test Question #1

What is a reasonable 4" pipe to select for a Class 3 distribution system with a MAOP of 400 psig?

- (1) 4", API 5-L Gr B, 0.120w, ERW
- (2) 4", API 5-L Gr B, 0.188w, ERW
- (3) 4", API 5-L X-42, 0.237w, ERW

## Steel Pipe Test Question #1

What is a reasonable 4" pipe to select for a Class 3 distribution system with a MAOP of 400 psig?

- (1) 4", API 5-L Gr B, 0.120w, ERW
- (2) 4", API 5-L Gr B, 0.188w, ERW
- (3) 4", API 5-L X-42, 0.237w, ERW

Solution (using Barlow's Formula to limit at 20% SMYS)

- (1) 4", API 5-L Gr B, 0.120w, ERW
  - $P = 2 \times (35,000 \times 0.20) \times 0.120 / 4.5 = 373 \text{ psig}$
- (2) 4", API 5-L Gr B, 0.188w, ERW
  - $P = 2 \times (35,000 \times 0.20) \times 0.188 / 4.5 = 584 \text{ psig}$  ← My Choice
- (3) 4", API 5-L X-42, 0.237w, ERW
  - $P = 2 \times (42,000 \times 0.20) \times 0.237 / 4.5 = 884 \text{ psig}$

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## Steel Pipe Test Question #2

I have an 8", 0.188w, unknown grade transmission pipe in a Class 3 location with a 575 psig MAOP. Is it OK from a pipe design standpoint?

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## Steel Pipe Test Question #2

I have an 8", 0.188w, unknown grade transmission pipe in a Class 3 location with a 575 psig MAOP. Is it OK from a pipe design standpoint?

Solution (using Design Formula)

$$P = 2 \times 24,000 \times 0.188 / 8.625 \times 0.50 \times 1.00 \times 1.00 = 523 \text{ psig NOPE}$$

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## Steel Pipe Test Question #3

What is 50% SMYS in a Class 1 location for 16", API 5L X-52, 0.250w, Butt Welded pipe?

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## Steel Pipe Test Question #3

What is 50% SMYS in a Class 1 location for 16", API 5L X-52, 0.250w, Butt Welded pipe?

Solution (using Barlow's Formula)

$$P = 2 \times (52,000 \times 0.50) \times 0.250 / 16 = 812 \text{ psig}$$

NOTE: 812 psig of internal pressure will create 50% SMYS for 16" API 5L X-52, 0.250w pipe regardless of class location, seam type, or temperature.



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## Steel Pipe Test Question #4

Is 12", API 5L GR B, 0.250w, ERW pipe suitable for a 300 psig MAOP Class 3 distribution pipeline?

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## Steel Pipe Test Question #4

Is 12", API 5L GR B, 0.250w, ERW pipe suitable for a 300 psig MAOP Class 3 distribution pipeline?

Solution (using Design Formula)

$$P = 2 \times 35,000 \times 0.250 / 12.75 \times 0.50 \times 1.00 \times 1.00 = 686.3 \text{ psig}$$

However, since distribution piping is limited to 20% SMYS, calculate "P" at 20% SMYS using Barlow's formula:

$$P = 2 \times (35,000 \times 0.20) \times 0.250 / 12.75 = 274.5 \text{ psig}$$

This pipe is suitable for a Class 3 design but is NOT suitable for a distribution pipeline since it would exceed 20% SMYS at 300 psig (causing it to be a transmission line)