



Hydrostatic Testing of Steel Pipelines

Ohio Gas Association
PHMSA Pipeline Safety Event
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Pressure Testing – Discussion Topics

- ▶ Focus: Hydrostatic Testing of Steel Pipelines & Facilities
- ▶ Pros and Cons
- ▶ Code Requirements
- ▶ Pressure Test Design
 - Establishment of Minimum & Maximum Test Pressures
- ▶ Pressure Test Operations
 - Filling & Stabilization
 - Testing & Documentation
 - Dewatering & Cleaning
- ▶ Record Keeping
- ▶ Environmental Permitting
- ▶ Safety Concerns

Pros and Cons

▶ Pros

Can be safer than pneumatic testing from an energy release perspective

Can be more cost effective than nitrogen, especially for large tests

Can be safer than natural gas (i.e. not flammable)

▶ Cons

Water can be difficult and expensive to obtain

Water can be difficult and expensive to dispose of

Costs associated with manpower and equipment used to fill, dewater, dry, etc.

Filling, stabilizing, dewatering, drying take additional time in project schedule

Water cannot always be completely removed

May be only option for high stress transmission lines



Pneumatic Test Failure



Hydrostatic Test Failure

Code Requirements

- ▶ §192.503 – General Requirements
 - a) No person may operate a new segment of pipeline, or return to service a segment of pipeline that has been relocated or replaced, until:
 - 1) It has been tested in accordance with this subpart [Subpart J] and §192.619 to substantiate the maximum allowable operating pressure; and
 - 2) Each potentially hazardous leak has been located and eliminated.
 - b) The test medium must be liquid, air, natural gas, or inert gas that is:
 - 1) Compatible with the material of which the pipeline is constructed;
 - 2) Relatively free of sedimentary materials; and
 - 3) Except for natural gas, nonflammable

Code Requirements

- ▶ §192.503 – General Requirements
 - c) Except as provided in §192.505(a), if air, natural gas, or inert gas is used as the test medium the following maximum hoop stress limitations apply:

Class Location	Maximum Hoop Stress as % SMYS	
	Natural Gas	Air or Inert Gas
1	80	80
2	30	75
3	30	50
4	30	40

Code Requirements

▶ §192.503 – General Requirements

- d) Each joint used to tie in a test segment of pipeline is excepted from the specific test requirements of this subpart, but each non-welded joint must be leak tested at not less than its operating pressure.
- e) If a component other than pipe is the only item being replaced or added to a pipeline, a strength test after installation is not required, if the manufacturer of the component certifies that:
 - 1) The component was tested to at least the pressure required for the pipeline to which it is being added.
 - 2) The component was manufactured under a quality control system that ensures that each item manufactured is at least equal in strength to a prototype and that the prototype was tested to at least the pressure required for the pipeline to which it is being added; or
 - 3) The component carries a pressure rating established through applicable ASME/ANSI, Manufacturers Standardization Society of the Valve and Fittings Industry, Inc. (MSS) specifications, or by unit strength calculations as described in §192.143.

Code Requirements

- ▶ §192.505 – Strength Tests for Steel Pipelines > 30% SMYS
 - a) ...each segment of a steel pipeline that is to operate at a hoop stress of 30 percent or more of SMYS must be strength tested in accordance with this section to substantiate the proposed maximum allowable operating pressure. In addition, in a Class 1 or Class 2 location, if there is a building intended for human occupancy within 300 feet of a pipeline, a hydrostatic test must be conducted to a test pressure of at least 125 percent of maximum operating pressure on that segment of the pipeline within 300 feet of such a building...
 - b) In a Class 1 or Class 2 location, each compressor station regulator station, and measuring station, must be tested to **at least Class 3** location test requirements.
 - c) Except as provided in paragraph (e) of this section, the strength test must be conducted by maintaining the pressure at or above the test pressure for **at least 8 hours**.
 - d) For fabricated units and short sections of pipe, for which a post installation test is impractical, a preinstallation strength test must be conducted by maintaining the pressure at or above the test pressure for at least 4 hours.

Code Requirements

▶ Hydrostatic Testing and Part 192

Hydrostatic testing and design incorporates multiple sections of Part 192

- Subpart A – General
 - §192.5 – Class Locations
- Subpart C – Pipe Design
- Subpart J – Test Requirements
- Subpart L – Operations
 - §192.619 – Maximum Allowable Operating Pressure (MAOP)

Hydrostatic Pressure Test Design

► Determination of Class Location

Class Location is a reflection of the population density and/or critical nature of the surrounding population

Class Location Unit: an area 220 yards on either side of the centerline of any continuous one mile length of pipeline

Class Locations:

- Class 1: Any class location unit that has 10 or fewer buildings IFHO
 - E.g. Rural countryside, sparsely populated
- Class 2: Any class location unit that has more than 10 but less than 46 buildings IFHO
 - E.g. Rural towns and villages

Hydrostatic Pressure Test Design

► Determination of Class Location (cont.)

Class Locations:

- Class 3: Any class location unit that has 46 or more buildings IFHO; or an area where the pipeline lies within 100 yards (300 feet) of either a small building or a small, well-defined outside area that is occupied by 20 or more persons on at least 5 days a week for 10 weeks in any 12-month period. The days and weeks need not be consecutive.
 - E.g. Large towns or cities; or stores, daycare facilities, schools, offices, parks, etc.
- Class 4: Any class location unit where buildings with four or more stories above ground are prevalent.
 - E.g. Downtown Columbus

Hydrostatic Pressure Test Design

► Determination of Minimum/Maximum Test Pressures

Minimum Test Pressure

- Established in accordance with §192.619(a)(2)(ii)
- The MAOP, for steel pipe operated at 100 psig or more, is calculated as “...the test pressure is divided by a factor determined in accordance with the following table:”

Class Location	Test Factor (Installed After Nov. 11, 1970)
1	1.10
2	1.25
3	1.50
4	1.50

- Note: Additional test factors are provided in 49 CFR Part 192 for pipelines being converted under §192.14 or installed prior to Nov. 11, 1970.

Hydrostatic Pressure Test Design

► Determination of Minimum/Maximum Test Pressures

Minimum Test Pressure

- IFHO's Within 300 feet
 - §192.505(a) states, "In addition, in a Class 1 or Class 2 location, if there is a building intended for human occupancy within 300 feet (91 meters) of a pipeline, a hydrostatic test must be conducted to a test pressure of at least 125 percent of maximum operating pressure on that segment of the pipeline within 300 feet (91 meters) of such a building..."
 - Additionally, "...if the buildings are evacuated while the hoop stress exceeds 50 percent of SMYS, air or inert gas may be used as the test medium."
 - Therefore, a test factor of 1.25 must be used on segments of the pipeline where there is a IFHO structure within 300 feet. This makes no difference on Class 2 locations, if hydrostatic testing is used, but does have an impact on Class 1 locations.

Hydrostatic Pressure Test Design

► Determination of Minimum/Maximum Test Pressures

Minimum Test Pressure

- Example: A pipeline has a design MAOP of **1,480 psig** and is located entirely within a **Class 1 Location** (Test Factor = **1.10** per §192.619(a)(2)(ii)). What is the minimum test pressure required, throughout the pipeline, to satisfy an MAOP of 1,480 psig?
- $1,480 \times 1.10 = 1,628$
- What if it was located in a Class 2 Location (Test Factor = **1.25** per §192.619(a)(2)(ii))?
- $1,480 \times 1.25 = 1,850$

Hydrostatic Pressure Test Design

► Determination of Minimum/Maximum Test Pressures

Maximum Test Pressure

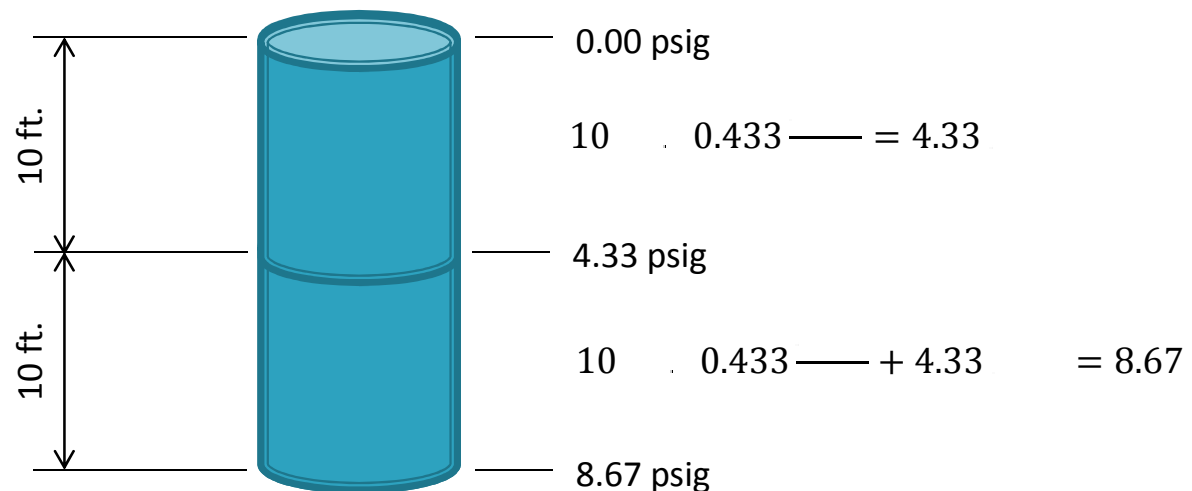
- Limited by safe operating pressure of components to be tested
 - Specified Minimum Yield Strength (SMYS) of Pipe
 - Example: 20" 0.375" WT Grade X52 API-5L PSL-2 Pipe SMYS = 1,950 psig
 - SMYS limitations vary by operator – UTI has seen 95% to 110% SMYS
 - Maximum Test Pressure of Component Ratings
 - ASME B16.5 (Flanges & Flanged Fittings), §2.6
 - “Flanged joints and flanged fittings may be subjected to system hydrostatic tests at a pressure of 1.5 times the 38°C (100°F) rating rounded off to the next higher 1 bar (25 psi) increment. Testing at any higher pressure is the responsibility of the user, taking into account the requirements of the applicable code or regulation.”
 - ANSI 600 Flange Pressure Rating = 1480 psig
 - Max. Test Pressure = $1.5 \times 1,480 = 2,220 \Rightarrow$ **2,225 psig** (next higher 25 psig increment)
 - UTI has seen instances where an operator obtains an approval letter from the manufacturer to allow a test pressure higher than that stated in ASME B16.5

Hydrostatic Pressure Test Design

► Pipeline Elevation Profile & Hydrostatic Head

Hydrostatic Head

- Water has a unit weight of 62.4 lbs/ft³
- Therefore, each foot of water in a column exhibits 62.4 lbs/ft² below it, or 0.433 lbs/in²
- This can be expressed as 0.433 psig / ft



Hydrostatic Pressure Test Design

► Pipeline Elevation Profile & Hydrostatic Head

Hydrostatic Head

- Example: If a pressure gauge on a pipeline filled with water reads 1,000 psig, what will the pressure be at a location, along the pipeline, 100 feet below?

- $1,000 + (100 \times 0.433) = 1,043.3$

- Likewise, what will the pressure be at a location 100 feet above?

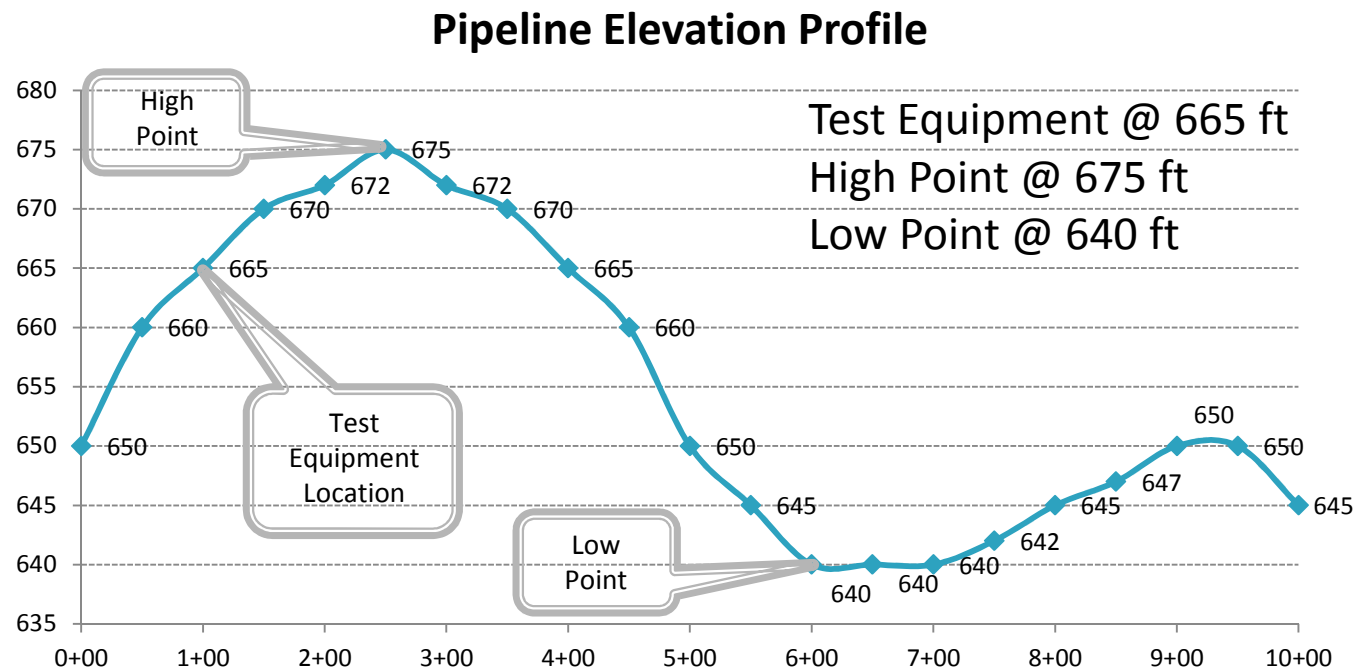
- $1,000 - (100 \times 0.433) = 956.7$

- Note: Hydrostatic Head is independent of slope of pipe, etc. It only matters how many vertical feet of water is below.

Hydrostatic Pressure Test Design

► Pipeline Elevation Profile & Hydrostatic Head

Example: An elevation profile is established for a pipeline that is ready to be tested.



Hydrostatic Pressure Test Design

► Pipeline Elevation Profile & Hydrostatic Head

Example (cont.):

Test Equipment @ 665 ft

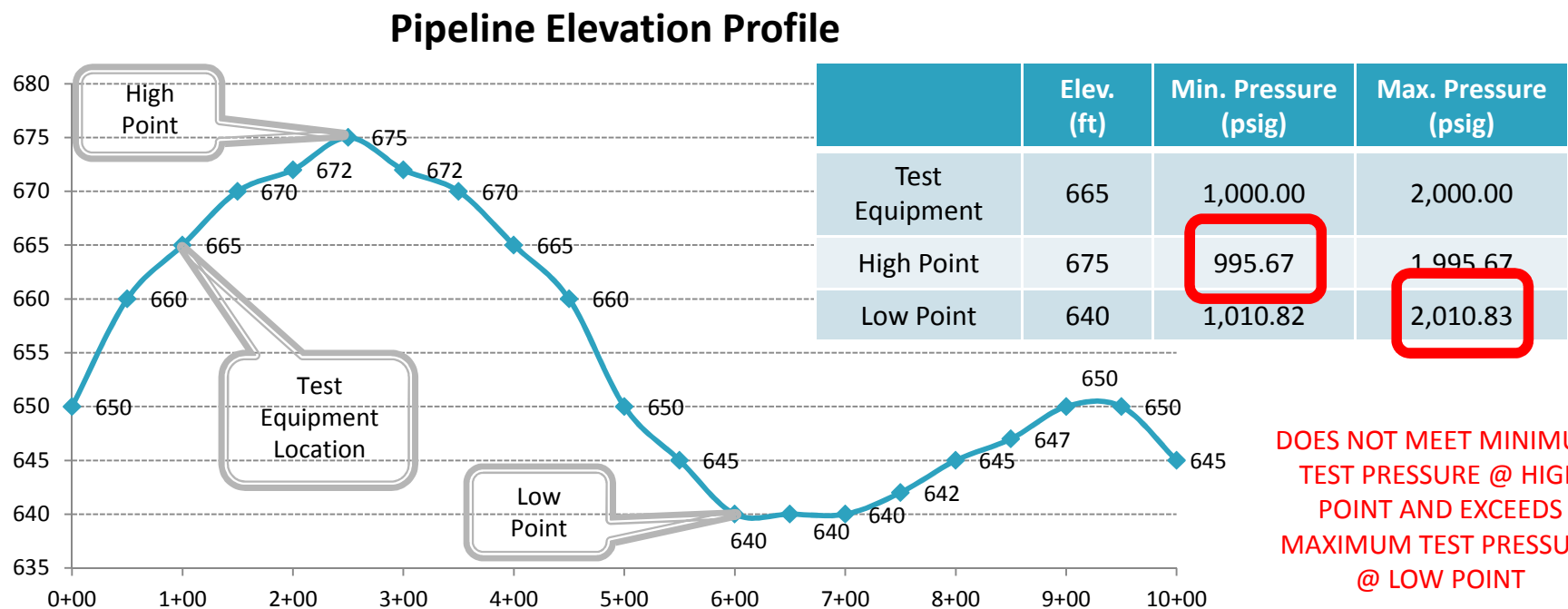
High Point @ 675 ft

Low Point @ 640 ft

- If we need to achieve a minimum pressure of 1,000 psig and are limited to a maximum pressure of 2,000 psig, what is the test range at the equipment location?
- Is it 1,000 psig to 2,000 psig? **WRONG**
- We need to adjust for elevation such that we:
 - a) Achieve the minimum test pressure at the peaks where pressure is the lowest, and
 - b) Stay below the maximum test pressure at the valleys, where pressure is the highest

Hydrostatic Pressure Test Design

- Pipeline Elevation Profile & Hydrostatic Head
Example (cont.):



Hydrostatic Pressure Test Design

► Pipeline Elevation Profile & Hydrostatic Head

Example (cont.):

- To determine what the minimum pressure will need to be at the test equipment, we need to work the process backwards.

	Elev. (ft)	Min. Pressure (psig)
Test Equipment	665	???
High Point	675	1,000.00

- What will the minimum test pressure need to be at the test equipment to achieve 1,000 psig minimum at the high point?
 - $$P_{Min} - (675 - 665) \times 0.433 = 1,000$$
 - Solve for P_{Min}
 - $$P_{Min} = 1,000 + 10 \times 0.433 = 1,004.33$$

Hydrostatic Pressure Test Design

► Pipeline Elevation Profile & Hydrostatic Head

Example (cont.):

	Elev. (ft)	Max. Pressure (psig)
Test Equipment	665	???
Low Point	640	2,000.00

- Likewise, what will the maximum test pressure need to be at the test equipment to not exceed the 2,000 psig maximum at the low point?

- $$P_{Max} - (640 - 665) \times 0.433 = 2,000$$

- Solve for P_{Max}

- $$P_{Max} = 2,000 + (-25) \times 0.433 = 1,989.17$$

Hydrostatic Pressure Test Design

► Pipeline Elevation Profile & Hydrostatic Head

Example (cont.):

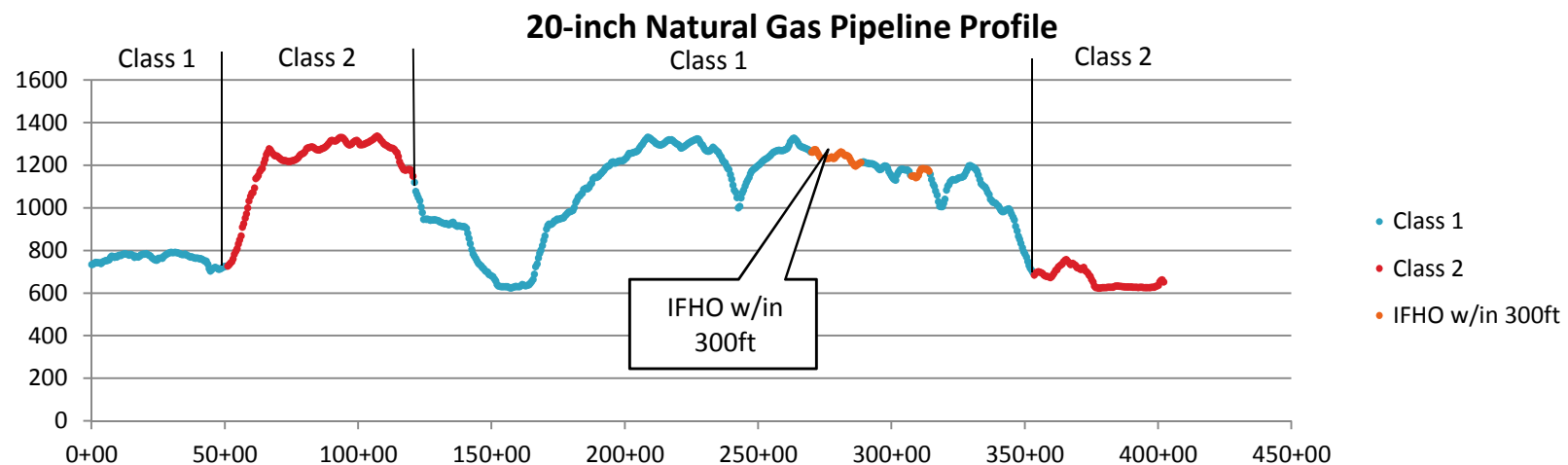
- When we reevaluate the table, we find that the adjusted pressure range at the test equipment satisfies the minimum pressure at the high point and the maximum pressure at the low point.

	Elev. (ft)	Min. Pressure (psig)	Max. Pressure (psig)
Test Equipment	665	1,004.33	1,989.18
High Point	675	1,000.00	1,984.85
Low Point	640	1,015.15	2,000.00

Hydrostatic Pressure Test Design

► Example Pipeline Pressure Test Design

A six mile 20-inch pipeline located in rural Ohio is being hydrostatically tested to meet the requirements of 49 CFR Part 192. The pipeline design MAOP is **1,440 psig** and features Class 1 and Class 2 locations as well as two areas where IFHO structures are within 300 feet.



Hydrostatic Pressure Test Design

► Example Pipeline Pressure Test Design

Location	Ground Elevation (ft)	Adjusted Elevation (ft)
Test Equipment	734	737 (+3ft)
Low Point, Class 1	624	614 (-10ft)
High Point, Class 1	1331	1328 (-3ft)
Low Point, Class 2	623	613 (-10ft)
High Point, Class 2	1337	1334 (-3ft)
Low Point, IFHO	1141	1135 (-4ft,-2ft)
High Point, IFHO	1273	1270 (-3ft)

Test Equipment adjusted by +3ft to account for chart recorder/gauge being above ground on table or other apparatus

Low Points adjusted by -10ft to account for bores under streams/roads/etc. and -4ft,-2ft for cover and diameter of pipe elsewhere

High Points adjusted by -3ft to account for minimum depth

If surveyed as-built elevation data of the pipeline and test equipment are available, utilize that data instead!

Hydrostatic Pressure Test Design

- ▶ Example Pipeline Pressure Test Design
- ▶ Minimum Test Pressure Determination

The Minimum Test Pressure, for Class 1 Location segments, is found to be:

$$\times 1.10 = 1,440 \quad \times 1.10 = 1,584$$

The Minimum Test Pressure, for Class 2 Location segments, is found to be:

$$\times 1.25 = 1,440 \quad \times 1.25 = 1,800$$

The Minimum Test Pressure, for segments with IFHO structures within 300 feet, is found to be:

$$\times 1.25 = 1,440 \quad \times 1.25 = 1,800$$

Hydrostatic Pressure Test Design

▶ Example Pipeline Pressure Test Design

▶ Minimum Test Pressure Adjusted for Elevation & Hydrostatic Head

The difference in elevation from the test equipment to the **highest** point within Class 1 Locations is:

- $1,328 \text{ feet} - 737 \text{ feet} = 591 \text{ feet}$
- $591 \text{ feet} \times 0.433 \text{ psig/ft} = 256 \text{ psig}$ (i.e. the pressure at the highest point will be 256 psig **less** than the pressure at the test equipment)

The difference in elevation from the test equipment to the **highest** point within Class 2 Locations is:

- $1,334 \text{ feet} - 737 \text{ feet} = 597 \text{ feet}$
- $597 \text{ feet} \times 0.433 \text{ psig/ft} = 259 \text{ psig}$ (i.e. the pressure at the highest point will be 259 psig **less** than the pressure at the test equipment)

The difference in elevation from the test equipment to the **highest** point within segments with IFHO structures within 300 feet is:

- $1,270 \text{ feet} - 737 \text{ feet} = 398 \text{ feet}$
- $533 \text{ feet} \times 0.433 \text{ psig/ft} = 231 \text{ psig}$ (i.e. the pressure at the highest point will be 231 psig **less** than the pressure at the test equipment)

Hydrostatic Pressure Test Design

- ▶ Example Pipeline Pressure Test Design
- ▶ Minimum Test Pressure Adjusted for Elevation & Hydrostatic Head

The minimum test pressure must be in excess of the minimum test pressure calculated at the highest elevation of the test sections.

Class 1 Locations:

- Minimum Test Pressure = 1,584 psig
- Adjusted Minimum Test Pressure at Test Equipment = $1,584 \text{ psig} + 256 \text{ psig} = 1,840 \text{ psig}$

Class 2 Locations:

- Minimum Test Pressure = 1,800 psig
- Adjusted Minimum Test Pressure at Test Equipment = $1,800 \text{ psig} + 259 \text{ psig} = 2,059 \text{ psig}$

Segments with IFHO Structures within 300 feet:

- Minimum Test Pressure = 1,800 psig
- Adjusted Minimum Test Pressure at Test Equipment = $1,800 \text{ psig} + 231 \text{ psig} = 2,031 \text{ psig}$

The Minimum Test Pressure, at the Test Equipment Location, shall be the largest of the adjusted minimum test pressures. Therefore, the minimum test pressure shall be **2,059 psig**.

Hydrostatic Pressure Test Design

- ▶ Example Pipeline Pressure Test Design
- ▶ Maximum Test Pressure Determination

Pipe Specifications

- 20" 0.375" WT X52 API-5L PSL-2 Pipe for Class 1 Location segments
- 20" 0.500" WT X60 API-5L PSL-2 Pipe for Class 2 Location segments

The SMYS of pipe, for Class 1 Location segments, is found to be:

$$\frac{2 \times 0.375}{1} = 0.75 = \frac{2 \times 0.375}{1} = 2,250$$

The pipe stress is limited to 100% of SMYS, therefore the Maximum Test Pressure is **2,250 psig**

The Maximum Test Pressure, for Class 2 Location segments, is found to be:

$$\frac{2 \times 0.500}{1} = 1.0 = \frac{2 \times 0.500}{1} = 3,000$$

The pipe stress is limited to 100% of SMYS, therefore the Maximum Test Pressure is **3,000 psig**

Hydrostatic Pressure Test Design

▶ Example Pipeline Pressure Test Design

▶ Maximum Test Pressure Adjusted for Elevation & Hydrostatic Head

The difference in elevation from the test equipment to the **lowest** point within Class 1 Locations is:

- 737 feet – 614 feet = 123 feet
- 123 feet x 0.433 psig/ft = 54 psig (i.e. the pressure at the lowest point will be 54 psig **more** than the pressure at the test equipment)

The difference in elevation from the test equipment to the **lowest** point within Class 2 Locations is:

- 737 feet – 613 feet = 124 feet
- 124 feet x 0.433 psig/ft = 54 psig (i.e. the pressure at the lowest point will be 54 psig **more** than the pressure at the test equipment)

The difference in elevation from the test equipment to the **lowest** point within segments with IFHO structures within 300 feet is:

- 737 feet – 1,135 feet = -398 feet
- -398 feet x 0.433 psig/ft = -172 psig (i.e. the pressure at the lowest point will be -172 psig **more** than the pressure at the test equipment)
- In this scenario, the lowest point on the segment is higher than the test equipment location

Hydrostatic Pressure Test Design

▶ Example Pipeline Pressure Test Design

▶ Maximum Test Pressure Adjusted for Elevation & Hydrostatic Head

The maximum test pressure must be below of the maximum test pressure calculated at the lowest elevation of the test sections.

Class 1 Locations:

- Maximum Test Pressure = 2,250 psig
- Adjusted Maximum Test Pressure at Test Equipment = $2,250 \text{ psig} - 54 \text{ psig} = 2,196 \text{ psig}$

Class 2 Locations:

- Maximum Test Pressure = 3,000 psig
- Adjusted Maximum Test Pressure at Test Equipment = $3,000 \text{ psig} - 54 \text{ psig} = 2,946 \text{ psig}$

Segments with IFHO Structures within 300 feet:

- Maximum Test Pressure = 2,250 psig
- Adjusted Maximum Test Pressure at Test Equipment = $2,250 \text{ psig} - (-172) \text{ psig} = 2,422 \text{ psig}$

The Maximum Test Pressure, at the Test Equipment Location, shall be the smallest of the adjusted maximum test pressures. Therefore, the maximum test pressure shall be **2,196 psig**.

Hydrostatic Pressure Test Design

- ▶ **Example Pipeline Pressure Test Design**
- ▶ Adjusted Test Range calculated to be 2,059 psig to 2,196 psig
- ▶ Typical test ranges for pipelines of this size have a 50 psig “window”
- ▶ UTI typically recommends testing on the higher end of the allowable test range
 - Higher test pressures increase chance to find fatal flaws in pipeline
 - Higher test pressures may aid in uprates and/or class location changes in the future
- ▶ **Miscellaneous Considerations:**
 - Accuracy of Data
 - Accuracy of elevation data should be considered. If the elevation data accuracy is known, the elevations should be adjusted accordingly in a conservative manner
 - Test Range Buffer
 - UTI typically provides a 10 psig buffer on either end of the test range as an additional measure of safety
- ▶ For this example, UTI would recommend a test pressure range (at the equipment) of **2,136 psig to 2,186 psig**
- ▶ **Note:** This scenario allowed a single test. Depending on elevation profile, a single test may not be viable unless stronger pipe is used.

Hydrostatic Pressure Test Design

▶ 90% SMYS Rule

Often companies will test to a minimum of 90% of the pipeline SMYS. Doing so will satisfy the requirements in §192.611 when a change in Class Location is found

§192.611 states that, when a Class Location is revised up (e.g. Class 1 to Class 2), the MAOP may remain unchanged assuming:

- The pipe design pressure still satisfies the design factor for the original Class Location; and
- The pipe test pressure satisfies the test factor for the new Class Location.
- Note applicable for changing to Class 4 Locations and the test factor is 1/0.555

The 90% SMYS Rule is a simplified method to ensure the pipe is tested to a test factor one Class Location higher than it is designed

Derivation:

$$\text{MAOP} = \text{SMYS} \times \text{DF}$$

$$\text{TP} = \text{MAOP} \times \text{TF}$$

$$\therefore \text{TP} = \text{SMYS} \times \text{DF} \times \text{TF}$$

For Class 1 designs, $\text{TP} = \text{SMYS} \times 0.72 \times 1.25 = \text{SMYS} \times 0.90$ or **90% SMYS**

For Class 2 designs, $\text{TP} = \text{SMYS} \times 0.60 \times 1.50 = \text{SMYS} \times 0.90$ or **90% SMYS**

Hydrostatic Pressure Test Design

- ▶ Spike Hydrostatic Testing

- Resulted from findings that hydrostatic testing is not effective in exposing defects along the circumference of the pipe (Michael Baker Jr., Inc., 2004)

- Additional measure for operators to expose defects in pipelines

- Not required by, nor does it directly satisfy 49 CFR Part 192

- Typical pressure test range of 100% to 110% of SMYS

- Typical duration of one (1) hour per AGA and CEPA (Canadian Energy Pipeline Association). ASME recommends only ten (10) minutes.

Hydrostatic Pressure Test Design

- ▶ UTI's Method for Test Design

- UTI utilizes a proprietary spreadsheet for calculating test ranges

- Allows for input of pipe/fitting/PRC specifications, elevations, etc.

- Greatly increases the speed of test design process

- Reduces potential for human error in test calculations, etc.

- Provides a neat, orderly form for records

- Greatly simplifies process of test design for complex pipelines with multiple classes, pipe specifications, and fittings/flanges/valves

Hydrostatic Pressure Test Operations

► Filling & Dewatering Pipelines

Filling

- Filling the pipeline with water should be done slowly and in a controlled manner to eliminate any shock to the system and remove any trapped air.
- Often pigs are pushed ahead to keep the water column intact to prevent mixing.
- The water can, especially on large diameter and/or long pipelines, take hours or days to stabilize.
- Often a chart is placed on the test header during fill to observe the stabilization.
- Water should be clean and free of debris. Depending on source & quality, water may require chemical treatment.
- Pressure up in stages to reduce shock to system. Allow to stabilize (overnight, when possible).

Hydrostatic Pressure Test Operations

► Filling & Dewatering Pipelines

Dewatering

- Dewatering the pipeline should be done slowly and in a controlled manner.
- Poly pigs and/or squeegee pigs are used to push the water towards the dewater location.
- Foam pigs are used to soak up any excess water remaining.

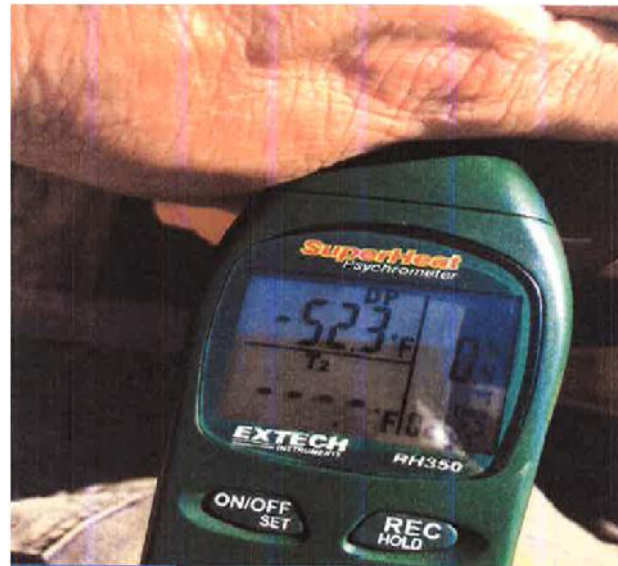


Hydrostatic Pressure Test Operations

► Filling & Dewatering Pipelines

Drying

- UTI typically specifies that pipelines are dried to -40 °F
- Contractors utilize dehydrated air compressors
- Dehydrated air is blown through entire pipeline with open-cell polyurethane pigs
- Wicks up any remaining moisture
- Verify dryness with calibrated digital hygrometer



Hydrostatic Pressure Test Operations

▶ Test Equipment Setup

A test header is often used to provide connections for the pump, gauges, charts, etc.

The test header materials must be verified prior to the test to ensure they can safely handle the proposed test range.

Test equipment, especially chart recorders, are vulnerable to excessive vibrations caused by equipment and personnel. All equipment should be placed in a location where it is mechanically isolated and not in danger of being bumped or otherwise disturbed.

Hoses and/or pipe to/from the test header and test equipment should be protected from equipment and personnel.

Additionally, hoses and/or pipe should be covered and/or insulated to prevent swings in temperature from the sun, rain, snow, etc.



Hydrostatic Pressure Test Operations

▶ Test Preparation

Verify test equipment location matches that shown on the test design

Verify pipe, fittings, flanges, valves, etc. in test

- Must match those described on test design
- Stop operation if material to be tested does not match test design

Verify all equipment calibrations and retain copies

- Serial numbers must match calibration records
- Calibration dates must be within acceptable time range

Verify all equipment is in good working order with new batteries, if applicable

Verify all equipment is connected properly

Step up pressure on pipeline, to the target test pressure, in multiple sections

- Hold after each step to allow stabilization and check for leaks
- Number of step ups and hold times are dependent on size of pipeline, among other factors

Step up to final target test pressure and disconnect all pumps

Begin test

Hydrostatic Pressure Test Operations

▶ Test Operation

UTI typically records pressure and temperature readings in fifteen minute increments

- Readings are relayed in real time to engineering and operations groups for continuous monitoring
- If any issues arise, they may be corrected or the test restarted immediately rather than delaying until the end of the test

Inspectors and/or contractors should check for leaks at various times throughout the test

- Check all visible locations, especially threaded and bolted connections
- Frequency of leak checks should be determined by the operator

Pumping and/or bleeding of pressure should not be permitted without approval and detailed documentation as to the reason

Upon completion but prior to depressurizing, inspectors send pressure readings and photos of charts to engineering and operations to verify test completeness and validity

Hydrostatic Pressure Test Operations

▶ Test Acceptance

In order to accept a hydrostatic pressure test, the following items should be considered:

- Test chart and/or pressure gauge depict pressures within the test range for a continuous eight (8) hours
- All equipment calibration records are current and accounted for
- No leaks were found, per §192.503(a)(2)
 - Any rise or fall in pressure **must** be able to be directly attributed to temperature, weather, precipitation, etc. (i.e. not a leak)
 - In cases where pressure drops are thought to be attributed to temperature, UTI's senior management and the client review all data and make the final determination (i.e. not inspection or contractors)
 - If no determination can be justified, the test may be extended until the pressure is observed to continuously and consistently rise (as temperatures increase)
 - UTI has found some operators will make a determination of no leaks if the test pressure is found to not fall over a continuous one (1) hour period. This could be followed up with a leak survey after commissioning as additional assurance.

Hydrostatic Pressure Test Operations

► Documentation & Record Keeping

Test records are the pedigree of the pipeline!

Per §192.517(a), “Each operator shall make, and retain for the useful life of the pipeline, a record of each test performed...”

Per the same section, the operator must retain the following information, at a minimum:

- The operator's name, the name of the operator's employee responsible for making the test, and the name of any test company used
- Test medium used
- Test pressure
- Test duration
- Pressure recording charts, or other record of pressure readings
- Elevation variations, whenever significant for the particular test
- Leaks and failures noted and their disposition

Hydrostatic Pressure Test Operations

► Documentation & Record Keeping

In addition, UTI recommends keeping the following records, where applicable

- Test equipment calibration records
- Test equipment makes and models
- Dates and times of readings
- Sign off from company, inspector, contractor, and engineering
- Notes of type of weather experienced and any noticeable affects on the test
- Drawings and/or detailed description of what was tested (especially when pipelines or facilities are tested in multiple segments and breakpoints are not obvious)

Environmental Permitting

▶ Water Supply & Disposal

Water from municipal water supplies ideal given high quality

- Permit or agreement typically required

Water from streams, ponds, etc. may introduce silt, sand, debris, and bacteria

- Permit may be required (e.g. ODNR water withdrawal permit)
- Debris can be strained out prior to introduction to pipeline
- Presence of bacteria requires chemical treating

Water discharged overland or back into streams

- Permit typically required (e.g. OEPA Hydrostatic Discharge Permit #OH000002)
- Water must be collected and tested
 - Requirements differ for new pipelines vs. used pipelines
- Environmental controls required to eliminate erosion

Water discharged to tanks and disposed of off site

- Water must be disposed of at approved site
- Can be less expensive and quicker process on smaller jobs

Safety Concerns

- ▶ **Communication**

- Personnel on site should have readily available means of communication with all other personnel involved

- Examples include radios, cellphones, line-of-sight, etc.

- ▶ **Boundaries & Barriers**

- Barriers, tape, fencing, etc. should be erected around the test area

- Stage personnel and/or erect signs at all points of ingress along the pipeline to warn of the test/restrict access

- All non-essential personnel and the public should be kept at a safe distance

- Only essential personnel should be allowed in the test area and should only remain there as needed to safely and effectively operate the test.

- In special circumstances, equipment may be used to act as a barrier between the test area and nearby structures

- ▶ **General Safety**

- Keep equipment in good, safe operating condition

- Keep hoses, pipes, etc. out of traveled areas, covered, or well marked to avoid tripping hazards



TOTAL CAPABILITIES IN THE PIPELINE INDUSTRY

QUESTIONS?

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